# **Predictive Data Science for physical systems**

From model reduction to scientific machine learning

Professor Karen E. Willcox Mathematics of Reduced Order Models | ICERM | 2-20-20<sup>2</sup>





## The Team

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1 Scientific Machine Learning What, Why & How?

### Outline

#### 2 Lift & Learn

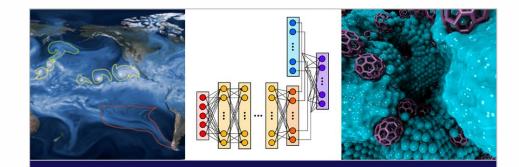
Projection-based model reduction as a lens through which to learn predictive models



### **Scientific Machine Learning**

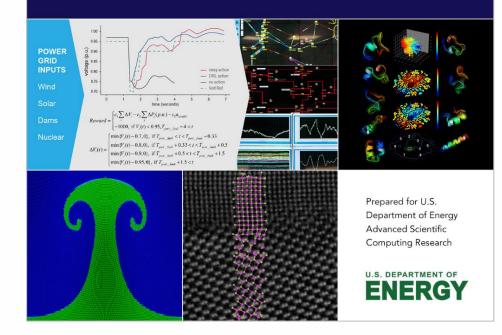
"Scientific machine learning (SciML) is a core component of artificial intelligence (AI) and a computational technology that can be trained, with scientific data, to augment or automate human skills.

Across the Department of Energy (DOE), SciML has the potential to transform science and energy research. Breakthroughs and major progress will be enabled by harnessing DOE investments in massive data from scientific user facilities, software for predictive models and algorithms, high-performance computing platforms, and the national workforce."



#### BASIC RESEARCH NEEDS FOR Scientific Machine Learning

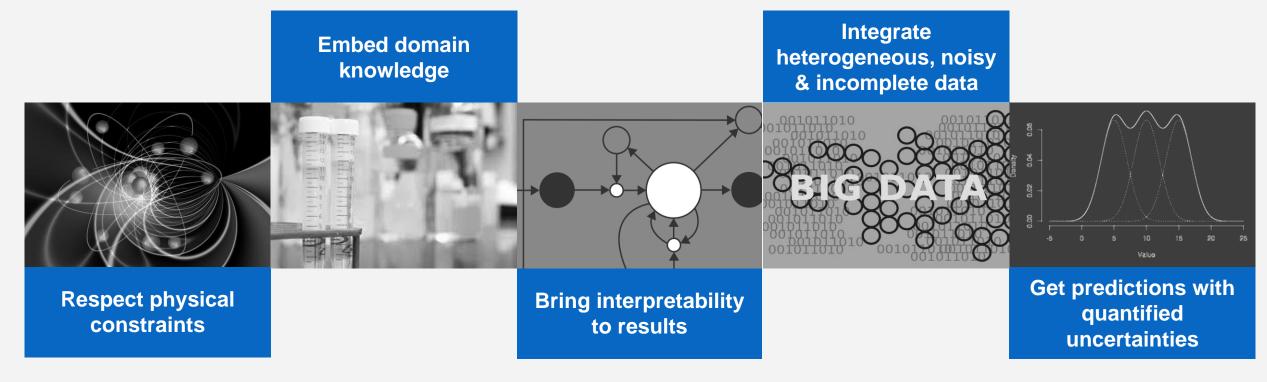
**Core Technologies for Artificial Intelligence** 



# Scientific Machine Learning

#### What role for model reduction?

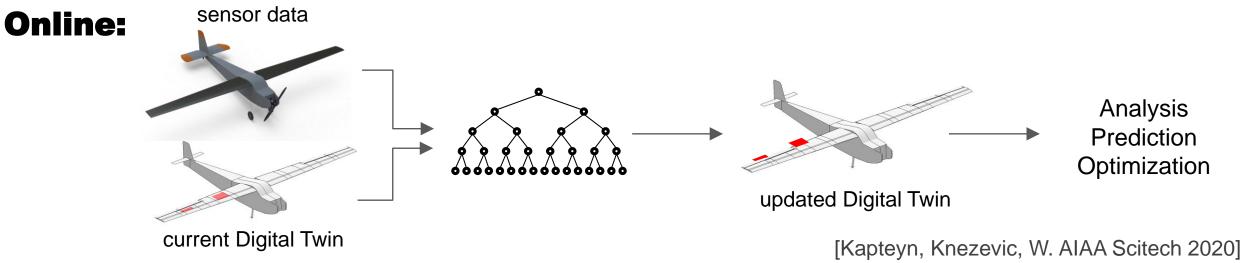
1 reduce the cost of training 2 foundational shift in ML perspectives



# **Predictive Digital Twin**

via component-based ROMs and interpretable machine learning ROMs embed predictive modeling and reduce the cost of training





#### **Machine learning**

"The scientific study of algorithms & statistical models that computer systems use to perform a specific task without using explicit instructions, relying on patterns & inference instead." [Wikipedia]

#### **Reduced-order modeling**

"Model order reduction (MOR) is a technique for reducing the computational complexity of mathematical models in numerical simulations." [Wikipedia]

# What is the connection between reduced-order modeling and machine learning?

Model reduction methods have grown from Computational Science & Engineering, with focus on *reducing* high-dimensional models that arise from physics-based modeling, whereas machine learning has grown from Computer Science, with a focus on *creating* low-dimensional models from black-box data streams. [Swischuk et al., *Computers & Fluids*, 2019]

#### **Machine learning**

"The scientific study of algorithms & statistical models that computer systems use to perform a specific task without using explicit instructions, relying on patterns & inference instead." [Wikipedia]

#### **Reduced-order modeling**

"Model order reduction (MOR) is a technique for reducing the computational complexity of mathematical models in numerical simulations." [Wikipedia]

### Reduced-order modeling & machine learning: Can we get the best of both worlds?

Discover hidden structure Non-intrusive implementation Black-box & flexible Accessible & available

Embed governing equations

Structure-preserving

Predictive (error estimators)

Stability-preserving

**1** Scientific Machine Learning

2 Lift & Learn

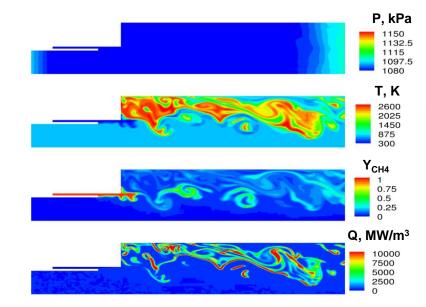
3 Conclusions & Outlook

# Lift & Learn

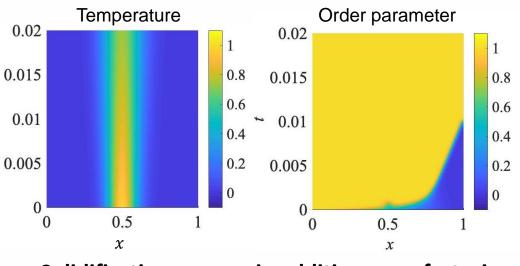
Projection-based model reduction as a lens through which to learn low-dimensional predictive models

## Lift & Learn: Ingredients

- 1. A **physics-based model** Typically described by a set of PDEs or ODEs
- 2. Lens of **projection** to define a structure-preserving low-dimensional model
- 3. Non-intrusive learning of the reduced model
- 4. Variable transformations that expose polynomial structure in the model
   → can be exploited with non-intrusive learning







+

Solidification process in additive manufacturing

## Start with a physics-based model

Example: modeling solidification in additive manufacturing Space/time evolution of temperature T and phase parameter  $\phi$ 

$$\dot{T} + L\dot{\phi} = \nabla. \left(K\left(\phi\right)\nabla T\right)$$
$$\alpha\xi^{2}\dot{\phi} = \xi^{2}\Delta\phi - p'\left(\phi\right) - q\left(T,\phi\right)$$

with

$$K(\phi) = K_0 (1 - h(\phi)) + K_1 h(\phi)$$
  

$$h(\phi) = 6\phi^5 - 15\phi^4 + 10\phi^3$$
  

$$p(\phi) = \frac{1}{4}\phi^2 (1 - \phi)^2 \qquad q(T, \phi) = \frac{\beta}{2}\phi(\phi - 1) \tanh[\gamma(T_{\text{melt}} - T)]$$

Model based on Kobayashi, 1993; collaboration with Bao & Biros

laser movement of laser melt pool powder lave solidified laver scanner system lase powder bed powder reservoi object being fabricated powder scraper powder delivery piston fabrication piston

Figure from: https://www.bintoa.com/powder-bed-fusion/

**Discretize**: Spatially discretized finite element model

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} + \mathbf{f}(\mathbf{x}, \mathbf{u})$$

discretized state x contains temperature and phase field order parameter at  $N_z$  spatial grid points

$$N_z \sim O(10^3 - 10^9)$$





## **Projection-based model reduction**

Train: Solve PDEs to generate training data (<u>snapshots</u>)
 Identify structure: Compute a <u>low-dimensional basis</u>
 Reduce: <u>Project</u> PDE model onto the low-dimensional subspace

Full-order model (FOM) state  $\mathbf{x} \in \mathbb{R}^N$ 

Reduced-order model (ROM) state  $\mathbf{x}_r \in \mathbb{R}^r$ 

#### $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$

Approximate $\mathbf{x} \approx \mathbf{V}\mathbf{x}_r$  $V \in \mathbb{R}^{N \times r}$ 

Residual:  $N \text{ eqs} \gg r \text{ dof}$ 

 $\mathbf{r} = \mathbf{V}\dot{\mathbf{x}}_r - \mathbf{A}\mathbf{V}\mathbf{x}_r - \mathbf{B}\mathbf{u}$ 

**Project**   $\mathbf{W}^{\top}\mathbf{r} = 0$ (Galerkin:  $\mathbf{W} = \mathbf{V}$ )

 $\dot{\mathbf{x}}_r = \mathbf{A}_r \mathbf{x}_r + \mathbf{B}_r \mathbf{u}$ 

Projecting a linear system

## Linear Model

FOM:  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$ 

**ROM:**  $\dot{\mathbf{x}}_r = \mathbf{A}_r \mathbf{x}_r + \mathbf{B}_r \mathbf{u}$ 

Precompute the ROM matrices:

 $\mathbf{A}_r = \mathbf{V}^\top \mathbf{A} \mathbf{V}, \ \mathbf{B}_r = \mathbf{V}^\top \mathbf{B}$ 

## **Quadratic Model**

**FOM:**  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{H}(\mathbf{x} \otimes \mathbf{x}) + \mathbf{B}\mathbf{u}$ 

**ROM:**  $\dot{\mathbf{x}}_r = \mathbf{A}_r \mathbf{x}_r + \mathbf{H}_r (\mathbf{x}_r \otimes \mathbf{x}_r) + \mathbf{B}_r \mathbf{u}$ 

Precompute the ROM matrices and tensor:

 $\mathbf{H}_r = \mathbf{V}^\top \mathbf{H} (\mathbf{V} \otimes \mathbf{V})$ 

projection preserves structure  $\leftrightarrow$  structure embeds physical constraints

## **Operator inference**

Non-intrusive learning of reduced models from simulation snapshot data

Given *reduced* state data, learn the *reduced* model

Operator Inference using proper orthogonal decomposition (POD) aka PCA

Peherstorfer & W. Data-driven operator inference for nonintrusive projection-based model reduction, *Computer Methods in Applied Mechanics and Engineering*, 2016

$$\dot{\widehat{\mathbf{x}}} = \widehat{\mathbf{A}}\widehat{\mathbf{x}} + \widehat{\mathbf{B}}\mathbf{u} + \widehat{\mathbf{H}}(\widehat{\mathbf{x}}\otimes\widehat{\mathbf{x}})$$

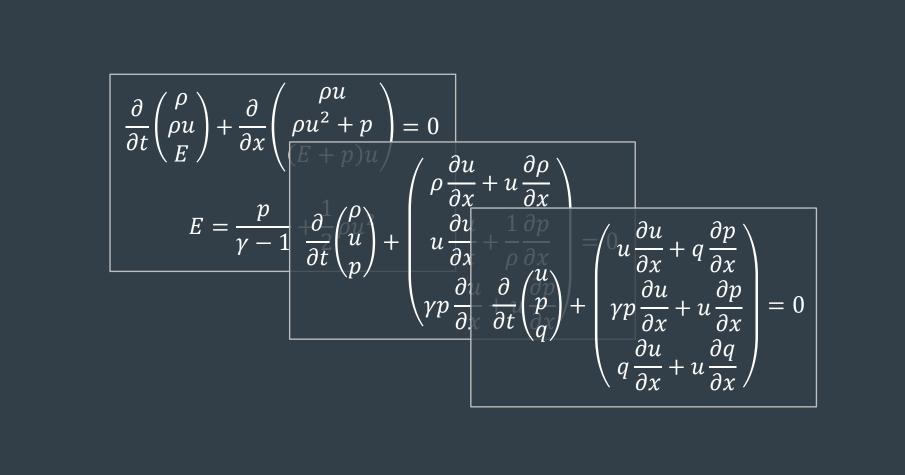
Given reduced state data ( $\widehat{\mathbf{X}}$ ) and derivative data ( $\widehat{\mathbf{X}}$ ):

$$\widehat{\mathbf{X}} = \begin{bmatrix} | & | \\ \widehat{\mathbf{x}}(t_1) & \dots & \widehat{\mathbf{x}}(t_K) \\ | & | \end{bmatrix} \qquad \dot{\widehat{\mathbf{X}}} = \begin{bmatrix} | & | \\ \dot{\widehat{\mathbf{x}}}(t_1) & \dots & \dot{\widehat{\mathbf{x}}}(t_K) \\ | & | \end{bmatrix}$$

Find the operators  $\widehat{A}$ ,  $\widehat{B}$ ,  $\widehat{H}$ by solving the least squares problem:

 $\min_{\widehat{A},\widehat{B},\widehat{H}} \left\| \widehat{X}^{\top} \widehat{A}^{\top} + \left( \widehat{X} \otimes \widehat{X} \right)^{\top} \widehat{H}^{\top} + \mathbf{U}^{\top} \widehat{B}^{\top} - \dot{\widehat{X}}^{\top} \right\|$ 

- Generate  $\widehat{\mathbf{X}}$  data by projection of  $\mathbf{X}$  snapshot data onto POD basis
- If data are Markovian, Operator Inference recovers the intrusive POD reduced model [Peherstorfer, 2019]



## Variable Transformations & Lifting

The physical governing equations reveal variable transformations and manipulations that expose polynomial structure

There are multiple ways to write the Euler equations

Different choices of variables leads to different **structure** in the discretized system

$$\frac{\partial}{\partial t} \begin{pmatrix} \rho \\ \rho w \\ E \end{pmatrix} + \frac{\partial}{\partial z} \begin{pmatrix} \rho w \\ \rho w^2 + p \\ (E+p)w \end{pmatrix} = 0$$
$$E = \frac{p}{\gamma - 1} + \frac{1}{2}\rho w^2$$

conservative variables mass, momentum, energy

$$\left| \begin{array}{c} \frac{\partial}{\partial t} \begin{pmatrix} \rho \\ w \\ p \end{pmatrix} + \begin{pmatrix} \rho \frac{\partial w}{\partial z} + w \frac{\partial \rho}{\partial z} \\ w \frac{\partial w}{\partial z} + \frac{1}{\rho} \frac{\partial p}{\partial z} \\ \gamma p \frac{\partial w}{\partial z} + w \frac{\partial p}{\partial z} \end{pmatrix} = 0 \right|$$

primitive variables mass, velocity, pressure

- Define specific volume:  $q = 1/\rho$
- Take derivative:  $\frac{\partial q}{\partial t} = \frac{-1}{\rho^2} \frac{\partial \rho}{\partial t} = \frac{-1}{\rho^2} \left( -\rho \frac{\partial u}{\partial z} u \frac{\partial \rho}{\partial z} \right) = q \frac{\partial u}{\partial z} u \frac{\partial q}{\partial z}$

$$\frac{\partial}{\partial t} \begin{pmatrix} w \\ p \\ q \end{pmatrix} + \begin{pmatrix} w \frac{\partial w}{\partial z} + q \frac{\partial p}{\partial z} \\ \gamma p \frac{\partial w}{\partial z} + w \frac{\partial p}{\partial z} \\ q \frac{\partial w}{\partial z} + w \frac{\partial q}{\partial z} \end{pmatrix} = 0$$

specific volume variables

$$\dot{\mathbf{x}} = \mathbf{H}(\mathbf{x} \otimes \mathbf{x}) + \mathbf{B}\mathbf{u}$$
transformed system
has quadratic structure

$$\dot{\mathbf{x}}_r = \mathbf{H}_r(\mathbf{x}_r \otimes \mathbf{x}_r) + \mathbf{B}_r \mathbf{u}$$

ROM has quadratic structure

Introducing auxiliary variables can expose structure → lifting

[McCormick 1976; Gu 2011]

- original state s(x, t)dimension  $d_s$
- lifted state w(x, t)dimension  $d_w$
- lifted PDE has quadratic form

Definition 1. Define the lifting map,

$$\mathcal{T}: \mathcal{S} \to \mathcal{W} \subset \mathbb{R}^{d_w}, \quad d_w \ge d_s, \tag{14}$$

and let  $w(x,t) = \mathcal{T}(s(x,t))$ .  $\mathcal{T}$  is a quadratic lifting of eq. (1) if the following conditions are met:

1. the map  $\mathcal{T}$  is differentiable with respect to s with bounded derivative, i.e., if  $\mathcal{J}(s)$  is the Jacobian of  $\mathcal{T}$  with respect to s, then

$$\sup_{s \in \mathcal{S}} \|\mathcal{J}(s)\| \le c,\tag{15}$$

for some c > 0, and

2. the lifted state w satisfies

$$\frac{\partial w}{\partial t} = a(w) + h(w), \tag{16}$$

where

$$a(w) = \begin{pmatrix} a_1(w) \\ \vdots \\ a_{d_w}(w) \end{pmatrix}, \qquad h(w) = \begin{pmatrix} h_1(w) \\ \vdots \\ h_{d_w}(w) \end{pmatrix}, \qquad (17)$$

for some linear functions  $a_j$  and quadratic functions  $h_j$ ,  $j = 1, 2, ..., d_w$ .

[Qian, Kramer, Peherstorfer, W. Physica D, 2020]

Introducing auxiliary variables can expose structure → lifting

[McCormick 1976; Gu 2011]

Example: Lifting a quartic ODE to quadratic-bilinear form

Can either lift to a system of ODEs or to a system of DAEs

Consider the quartic system

Introduce auxiliary variables:

Chain rule:

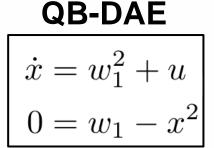
$$\dot{x} = x^4 + u_1$$

$$w_1 = x^2 \quad w_2 = w_1^2$$

$$\dot{w}_1 = 2x[w_1^2 + u] = 2x[w_2 + u]$$
$$\dot{w}_2 = 2w_1\dot{w}_1 = 4xw_1[w_2 + u]$$

Need additional variable to make auxiliary dynamics quadratic:  $w_3 = xw_1$   $\dot{w}_3 = \dot{x}w_1 + x\dot{w}_1$   $= w_1w_2 + w_1u + 2w_1w_2 + 2w_1u$ QB-ODE  $\dot{x} = w_2 + u$  QB-DAE

$$\dot{w}_1 = 2xw_2 + 2xu$$
$$\dot{w}_2 = 4w_2w_3 + 4w_3u$$
$$\dot{w}_3 = 3w_1w_2 + 3w_1u$$



### Many different forms of nonlinear PDEs can be lifted to polynomial form

$$\dot{T} + L\dot{\phi} = \nabla. \left(K\left(\phi\right)\nabla T\right)$$
$$\alpha\xi^{2}\dot{\phi} = \xi^{2}\Delta\phi - p'\left(\phi\right) - q\left(T,\phi\right)$$

original equations

$$\begin{split} \dot{T} + L\dot{\phi} &= \nabla . (K\nabla T) \\ \alpha \xi^2 \dot{\phi} &= \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \\ \dot{K} &= \frac{120 \left( K_1 - K_0 \right)}{\alpha \xi^2} p \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right] \\ \dot{p} &= \frac{1}{\alpha \xi^2} p' \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right] \\ \dot{p}' &= \frac{1}{\alpha \xi^2} p'' \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right] \\ \dot{p}'' &= \frac{3}{\alpha \xi^2} \left( 2\phi - 1 \right) \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right] \\ \dot{m}_0 &= -\gamma y \left\{ \nabla . \left( K \nabla T \right) - \frac{L}{\alpha \xi^2} \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right] \right\} \\ y &= 1 - m_0^2 \end{split}$$
 cubic lifted equations

[Khodabakhshi, W. In preparation.]

 $\begin{bmatrix} T \\ \phi \end{bmatrix}$ 

Nonlinear system for 1D solidification

$$\dot{T} + L\dot{\phi} = \nabla . \left(K\left(\phi\right)\nabla T\right)$$
$$\alpha\xi^{2}\dot{\phi} = \xi^{2}\Delta\phi - p'\left(\phi\right) - q\left(T,\phi\right)$$

with 
$$K(\phi) = K_0 (1 - h(\phi)) + K_1 h(\phi)$$
  
 $h(\phi) = 6\phi^5 - 15\phi^4 + 10\phi^3$   
 $p(\phi) = \frac{1}{4}\phi^2 (1 - \phi)^2$   
 $q(T, \phi) = \frac{\beta}{2}\phi (\phi - 1) \tanh [\gamma (T_{melt} - T)]$ 

DebRoy et al. Progress in Materials Science, 2018

 $\begin{bmatrix} T \\ \phi \end{bmatrix}$ 

Nonlinear system for 1D solidification

$$\dot{T} + L\dot{\phi} = \nabla. \left(K\left(\phi\right)\nabla T\right)$$
$$\alpha\xi^{2}\dot{\phi} = \xi^{2}\Delta\phi - p'\left(\phi\right) - q\left(T,\phi\right)$$

with  $K(\phi) = K_0 (1 - h(\phi)) + K_1 h(\phi)$   $h(\phi) = 6\phi^5 - 15\phi^4 + 10\phi^3$   $p(\phi) = \frac{1}{4}\phi^2 (1 - \phi)^2$  $q(T, \phi) = \frac{\beta}{2}\phi (\phi - 1) \tanh [\gamma (T_{melt} - T)]$ 

Chain rule:  $K = K_0 [1 - h(\phi)] + K_1 h(\phi)$   $\dot{K} = (K_1 - K_0) h'(\phi) \dot{\phi}$  $= \frac{120 (K_1 - K_0)}{\alpha \xi^2} p [\xi^2 \Delta \phi - p'(\phi) - q(T, \phi)]$ 

 $\begin{bmatrix} T \\ \phi \\ K \end{bmatrix}$ 

Nonlinear system for 1D solidification

$$\dot{T} + L\dot{\phi} = \nabla . (K\nabla T)$$
  

$$\alpha \xi^2 \dot{\phi} = \xi^2 \Delta \phi - p'(\phi) - q(T,\phi)$$
  

$$\dot{K} = \frac{120(K_1 - K_0)}{\alpha \xi^2} p \left[\xi^2 \Delta \phi - p'(\phi) - q(T,\phi)\right]$$

with 
$$p(\phi) = \frac{1}{4}\phi^2 (1-\phi)^2$$
  
 $q(T,\phi) = \frac{\beta}{2}\phi(\phi-1) \tanh[\gamma(T_{melt}-T)]$ 

$$p = \frac{1}{4}\phi^2 (1 - \phi)^2$$
$$\dot{p} = p'(\phi) \dot{\phi} = \frac{1}{\alpha\xi^2} p' \left[\xi^2 \Delta \phi - p'(\phi) - q(T, \phi)\right]$$

 $\begin{array}{c}
T \\
\phi \\
K
\end{array}$  $\lfloor p \rfloor$ 

Nonlinear system for 1D solidification

$$\dot{T} + L\dot{\phi} = \nabla . (K\nabla T)$$

$$\alpha \xi^2 \dot{\phi} = \xi^2 \Delta \phi - p'(\phi) - q(T,\phi)$$

$$\dot{K} = \frac{120 (K_1 - K_0)}{\alpha \xi^2} p \left[\xi^2 \Delta \phi - p'(\phi) - q(T,\phi)\right]$$

$$\dot{p} = \frac{1}{\alpha \xi^2} p' \left[\xi^2 \Delta \phi - p'(\phi) - q(T,\phi)\right]$$

with 
$$q(T,\phi) = \frac{\beta}{2}\phi(\phi-1) \tanh\left[\gamma\left(T_{\text{melt}}-T\right)\right]$$

$$p' = \frac{1}{2}\phi (1 - \phi) (1 - 2\phi)$$
$$\dot{p'} = p''(\phi) \dot{\phi} = \frac{1}{\alpha\xi^2} p'' \left[\xi^2 \Delta \phi - p'(\phi) - q(T, \phi)\right]$$



Nonlinear system for 1D solidification

$$\begin{split} \dot{T} + L\dot{\phi} &= \nabla.\left(K\nabla T\right) \\ \alpha\xi^{2}\dot{\phi} &= \xi^{2}\Delta\phi - p' - q\left(T,\phi\right) \\ \dot{K} &= \frac{120\left(K_{1} - K_{0}\right)}{\alpha\xi^{2}}p\left[\xi^{2}\Delta\phi - p' - q\left(T,\phi\right)\right] \\ \dot{p} &= \frac{1}{\alpha\xi^{2}}p'\left[\xi^{2}\Delta\phi - p' - q\left(T,\phi\right)\right] \\ \dot{p'} &= \frac{1}{\alpha\xi^{2}}p''\left[\xi^{2}\Delta\phi - p' - q\left(T,\phi\right)\right] \end{split}$$

with 
$$q(T,\phi) = rac{eta}{2}\phi(\phi-1) anh\left[\gamma\left(T_{ ext{melt}}-T
ight)
ight]$$

$$p'' = 3(\phi^2 - \phi) + \frac{1}{2}$$
$$\dot{p''} = 3(2\phi - 1)\dot{\phi} = \frac{3}{\alpha\xi^2}(2\phi - 1)[\xi^2\Delta\phi - p' - q(T, \phi)]$$



Nonlinear system for 1D solidification

$$\begin{split} \dot{T} + L\dot{\phi} &= \nabla. \left(K\nabla T\right) \\ \alpha\xi^{2}\dot{\phi} &= \xi^{2}\Delta\phi - p' - \frac{\beta}{6}\left(p'' - \frac{1}{2}\right)m_{0}\left(T\right) \\ \dot{K} &= \frac{120\left(K_{1} - K_{0}\right)}{\alpha\xi^{2}}p\left[\xi^{2}\Delta\phi - p' - \frac{\beta}{6}\left(p'' - \frac{1}{2}\right)m_{0}\left(T\right)\right] \\ \dot{p} &= \frac{1}{\alpha\xi^{2}}p'\left[\xi^{2}\Delta\phi - p' - \frac{\beta}{6}\left(p'' - \frac{1}{2}\right)m_{0}\left(T\right)\right] \\ \dot{p}' &= \frac{1}{\alpha\xi^{2}}p''\left[\xi^{2}\Delta\phi - p' - \frac{\beta}{6}\left(p'' - \frac{1}{2}\right)m_{0}\left(T\right)\right] \\ \dot{p}'' &= \frac{3}{\alpha\xi^{2}}\left(2\phi - 1\right)\left[\xi^{2}\Delta\phi - p' - \frac{\beta}{6}\left(p'' - \frac{1}{2}\right)m_{0}\left(T\right)\right] \end{split}$$

$$\begin{split} m_0 &= \tanh\left[\gamma \left(T_{\text{melt}} - T\right)\right] \\ \dot{m}_0 &= -\gamma \left(1 - m_0^2\right) \dot{T} \\ &= -\gamma \left(1 - m_0^2\right) \left\{\nabla \left(K \nabla T\right) - \frac{L}{\alpha \xi^2} \left[\xi^2 \Delta \phi - p' - \frac{\beta}{6} \left(p'' - \frac{1}{2}\right) m_0\right] \right\} \end{split}$$

Original system:

$$\dot{T} + L\dot{\phi} = \nabla. \left(K\left(\phi\right)\nabla T\right)$$
$$\alpha\xi^{2}\dot{\phi} = \xi^{2}\Delta\phi - p'\left(\phi\right) - q\left(T,\phi\right)$$

with original variables  $T, \phi$ 

Nonlinear system for 1D solidification

$\dot{T} + L\dot{\phi} = \nabla. (K\nabla T)$	Quadr	ratic
$\alpha \xi^2 \dot{\phi} = \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0$	Quadr	atic
$\dot{K} = \frac{120 \left(K_1 - K_0\right)}{\alpha \xi^2} p \left[\xi^2 \Delta \phi - p' - \frac{\beta}{6} \left(p'' - \frac{1}{2}\right) m_0\right]$	Cı	ubic
$\dot{p} = \frac{1}{\alpha\xi^2} p' \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{1}{2} \right) m_0 \right]$	Cı	ubic
$\dot{p'} = \frac{1}{\alpha\xi^2} p'' \left[\xi^2 \Delta \phi - p' - \frac{\beta}{6} \left(p'' - \frac{1}{2}\right) m_0\right]$	Cı	ubic
$\dot{p''} = \frac{3}{\alpha\xi^2} \left(2\phi - 1\right) \left[\xi^2 \Delta \phi - p' - \frac{\beta}{6} \left(p'' - \frac{1}{2}\right) m_0\right]$	Cı	ubic
$\dot{m}_0 = -\gamma y \left\{ \nabla . \left( K \nabla T \right) - \frac{L}{\alpha \xi^2} \left[ \xi^2 \Delta \phi - p' - \frac{\beta}{6} \left( p'' - \frac{\beta}{6} \right) \right] \right\}$	$\left[\frac{1}{2}\right)m_0\bigg]\bigg\}$ Cu	ubic
$y = 1 - m_0^2$	Quadr	atic

with lifted variables  $T, \phi, K, p, p', p'', m_0, y$ 

## Lift & Learn

Variable transformations to expose structure+ non-intrusive learning that frees us to choose our variables

Using only snapshot data from the original high-fidelity model (non-intrusive) but using variable transformations to expose and exploit structure

#### Lift & Learn [Qian, Kramer, Peherstorfer & W., 2019]

 Generate full state trajectories (snapshots) (from high-fidelity simulation)

$$\mathbf{X}_{\mathbf{orig}} = \begin{bmatrix} | & & | \\ \mathbf{x}(t_1) & \dots & \mathbf{x}(t_K) \\ | & & | \end{bmatrix} \quad \dot{\mathbf{X}}_{\mathbf{orig}} = \begin{bmatrix} | & & | \\ \dot{\mathbf{x}}(t_1) & \dots & \dot{\mathbf{x}}(t_K) \\ | & & | \end{bmatrix}$$

Using only snapshot data from the original high-fidelity model (non-intrusive) but using variable transformations to expose and exploit structure Lift & Learn [Qian, Kramer, Peherstorfer & W., 2019]

- Generate full state trajectories (snapshots) (from high-fidelity simulation)
- 2. Transform snapshot data to get lifted snapshots (analyze the PDEs to expose system polynomial structure)

$$X_{orig} \rightarrow X$$
  $\dot{X}_{orig} \rightarrow \dot{X}$ 

Using only snapshot data from the original high-fidelity model (non-intrusive) but using variable transformations to expose and exploit structure Lift & Learn [Qian, Kramer, Peherstorfer & W., 2019]

- Generate full state trajectories (snapshots) (from high-fidelity simulation)
- 2. Transform snapshot data to get lifted snapshots
- 3. Compute POD basis from lifted trajectories

 $\mathbf{X} = \mathbf{V} \, \boldsymbol{\Sigma} \, \mathbf{W}^{\top}$ 

Using only snapshot data from the original high-fidelity model (non-intrusive) but using variable transformations to expose and exploit structure

#### Lift & Learn [Qian, Kramer, Peherstorfer & W., 2019]

- Generate full state trajectories (snapshots) (from high-fidelity simulation)
- 2. Transform snapshot data to get lifted snapshots
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- 4. Project lifted trajectories onto POD basis, to obtain trajectories in low-dimensional POD coordinate space

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$$\min_{\widehat{\mathbf{A}},\widehat{\mathbf{B}},\widehat{\mathbf{H}}} \left\| \widehat{\mathbf{X}}^{\top} \widehat{\mathbf{A}}^{\top} + \left( \widehat{\mathbf{X}} \otimes \widehat{\mathbf{X}} \right)^{\top} \widehat{\mathbf{H}}^{\top} + \mathbf{U}^{\top} \widehat{\mathbf{B}}^{\top} - \dot{\widehat{\mathbf{X}}}^{\top} \right\|$$

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#### Lift & Learn [Qian, Kramer, Peherstorfer & W., 2019]

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Under certain conditions, recovers the intrusive POD reduced model

→ convenience of black-box learning + rigor of projection-based reduction + structure imposed by physics **1** Scientific Machine Learning

2 Lift & Learn

3 Conclusions & Outlook

# Additive Manufacturing

Lift & Learn reduced models for a highly nonlinear solidification process

# Modeling solidification in additive manufacturing

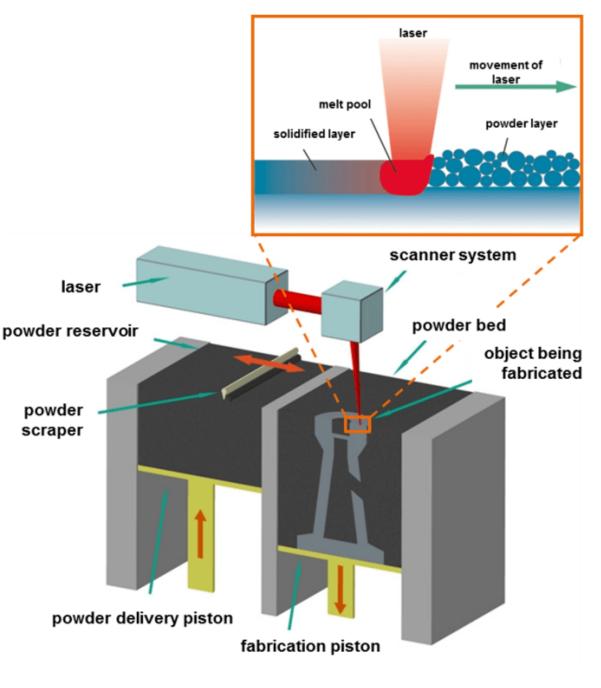
 $\dot{T} + L\dot{\phi} = \nabla . \left( K\left(\phi\right) \nabla T \right)$  $\alpha \xi^{2} \dot{\phi} = \xi^{2} \Delta \phi - p'\left(\phi\right) - q\left(T,\phi\right)$ 

- Spatial domain discretized into 1,000 cells
- Initial conditions

$$T(x,0) = 0.4$$
  
 $\phi(x,0) = 0.5 \cos(\pi x) + 0.5$ 

Boundary conditions

$$T(0,t) = T(\ell,t) 0.4$$
$$\frac{\partial \phi}{\partial x}\Big|_{x=0} = \frac{\partial \phi}{\partial x}\Big|_{x=\ell} = 0$$



https://www.bintoa.com/powder-bed-fusion

# Modeling solidification in additive manufacturing

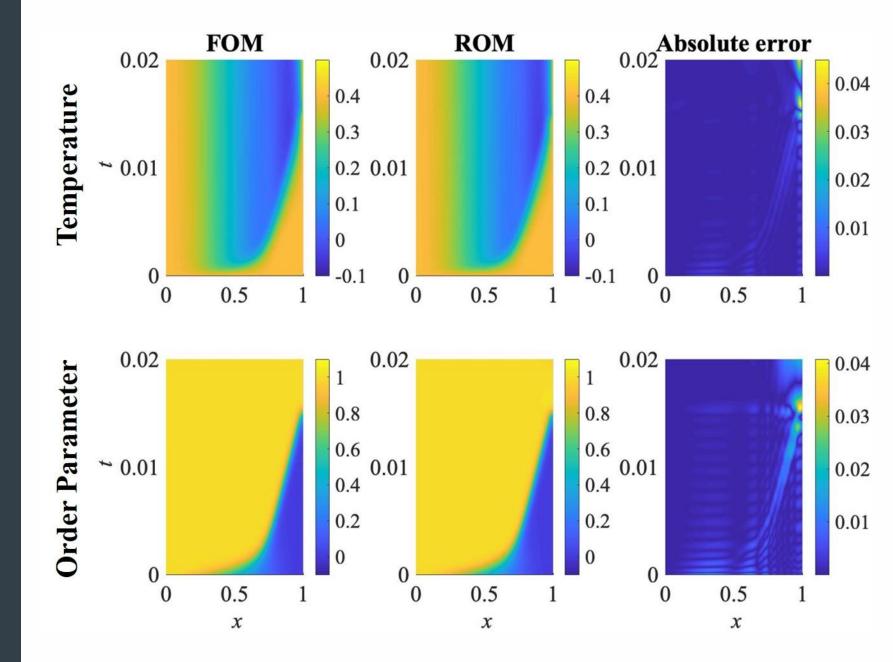
 $\dot{T} + L\dot{\phi} = \nabla . \left( K\left(\phi\right) \nabla T \right)$  $\alpha \xi^{2} \dot{\phi} = \xi^{2} \Delta \phi - p'\left(\phi\right) - q\left(T,\phi\right)$ 

#### **Training data**

- 800 snapshots collected over time t = [0, 0.02]
- Parameters:  $\ell = 1, \alpha = 3, \xi = 0.1, \beta = 0.9,$  $T_{\text{melt}} = 1.0, L = 0.5, \gamma = 2.0, K_0 = 1, K_1 = 0.1$
- Variables used for learning cubic ROMs  $\mathbf{x} = [T, \phi, K, p, p', p'', m_0, y]$

Lift & Learn reduced model performance

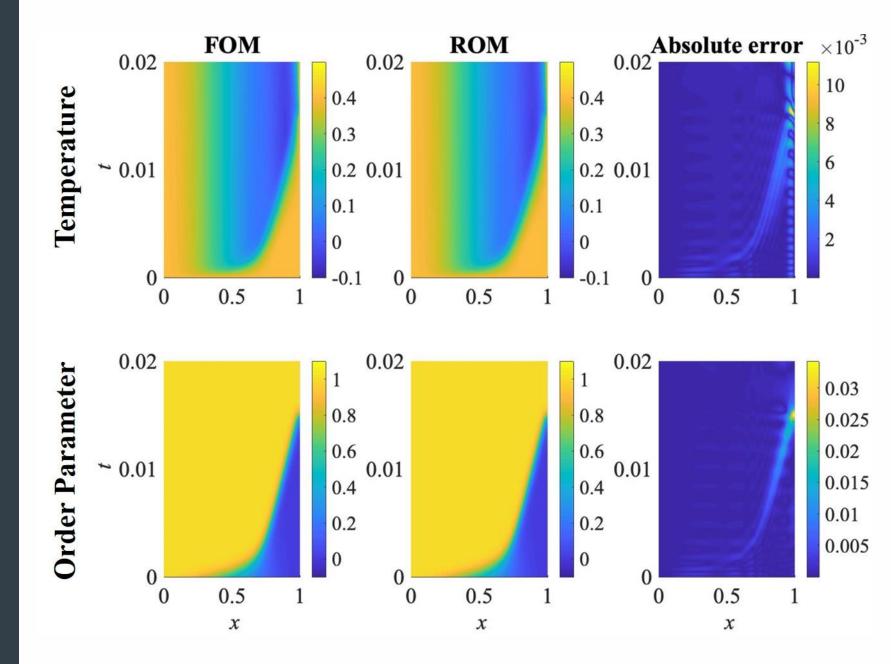
- r=23 POD basis functions
- 16 modes for differential eqs + 7 modes for algebraic eqs



Lift & Learn reduced model performance

• r= 32 POD basis functions

 22 modes for differential eqs + 10 modes for algebraic eqs



2 Lift & Learn

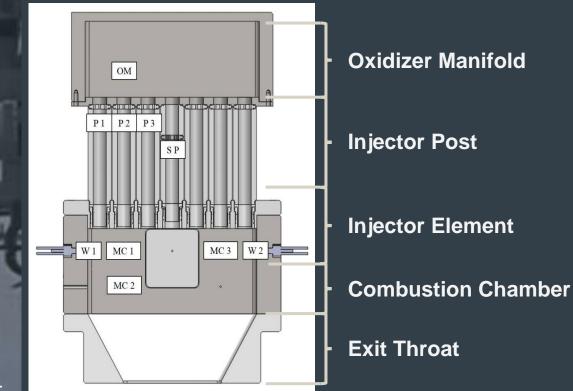
3 Conclusions & Outlook

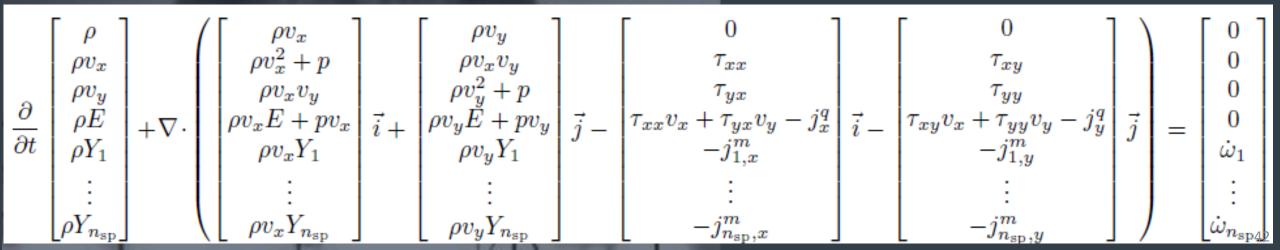
## Rocket Engine Combustion

Lift & Learn reduced models for a complex Air Force combustion problem

# Modeling a single injector of a rocket engine combustor

- Spatial domain (2D) discretized into 38,523 cells
- Oxidizer input: 0.37  $\frac{\text{kg}}{\text{s}}$  of 42%  $\text{O}_2$  / 58%  $\text{H}_2\text{O}$
- Fuel input: 5.0  $\frac{\text{kg}}{\text{s}}$  of CH<sub>4</sub>
- Forced by a back pressure boundary condition at exit throat

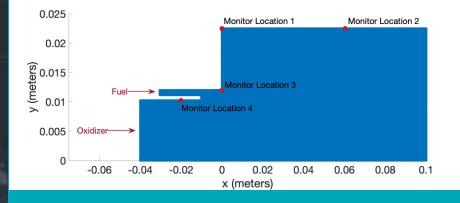




## Modeling a single injector of a rocket engine combustor

#### Training data

- 1 ms of full state solutions generated using Air Force GEMS code (~200 hours CPU time)
- Timestep  $\Delta t = 10^{-7}$ s; 10,000 total snapshots
- Variables used for learning ROMs  $\mathbf{x} = \begin{bmatrix} \mathbf{p} & \mathbf{u} & \mathbf{v} & \mathbf{1}/\rho & \rho Y_{CH_4} & \rho Y_{O_2} & \rho Y_{CO_2} & \rho Y_{H_2O} \end{bmatrix}$ makes many (but not all) terms in governing equations quadratic
- Snapshot matrix  $\mathbf{X} \in \mathbb{R}^{308,184 \times 10,000}$

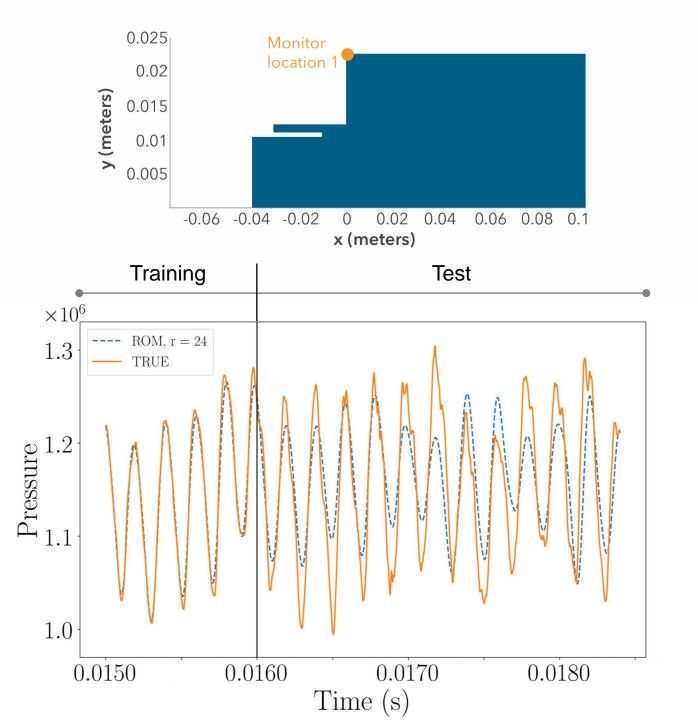


#### **Test data**

Additional 2 ms of data at four monitor locations (20,000 timesteps) Performance of learned quadratic ROM

Pressure time traces at monitor location 1

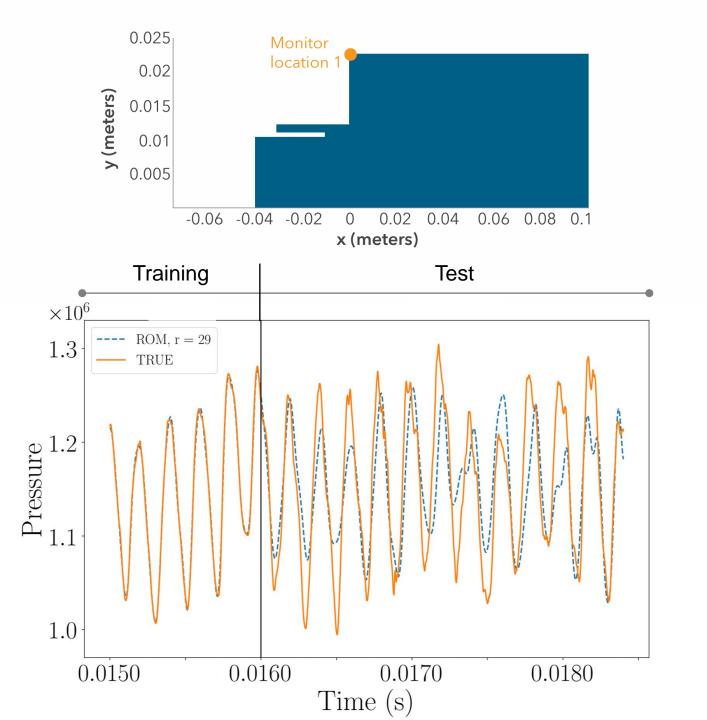
Basis size r = 24



Performance of learned quadratic ROM

Pressure time traces at monitor location 1

Basis size r = 29



True

#### Pressure

0.03

0.02

0.01

0

0

#### Temperature

0.1

К 2500

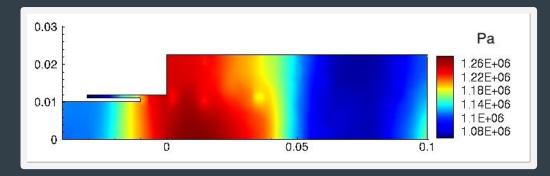
2000

1500

1000

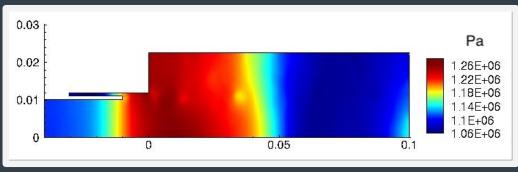
500

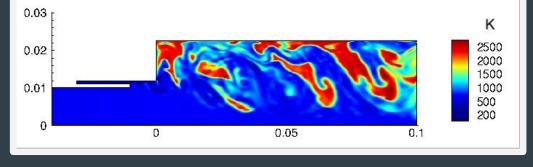
200



#### Predicted

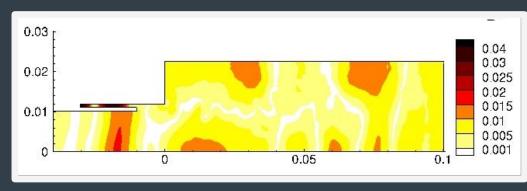
r = 29 POD modes

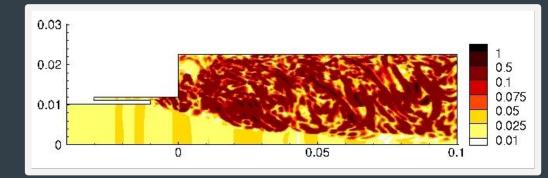




0.05

#### **Relative error**

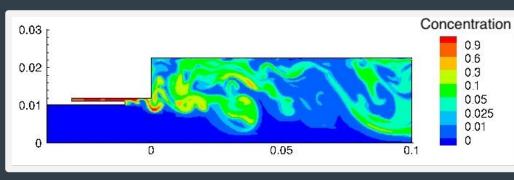




46

True

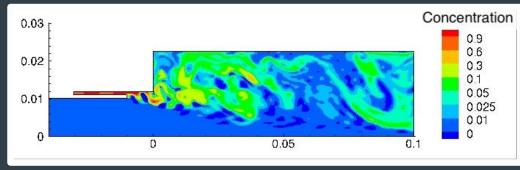
 $CH_4$ 

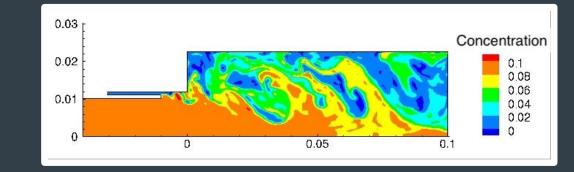


#### 0.03 0.02 0.01 0.01 0.02 0.05 0.01 0.01 0.02 0.02 0.02

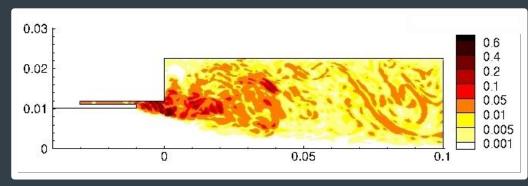
Predicted

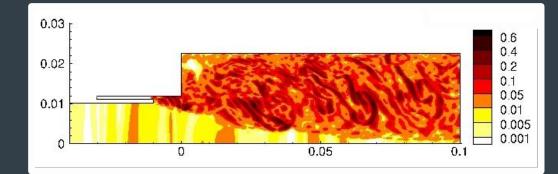
r = 29 POD modes





#### Normalized absolute error





**O**<sub>2</sub>

47

2 Lift & Learn

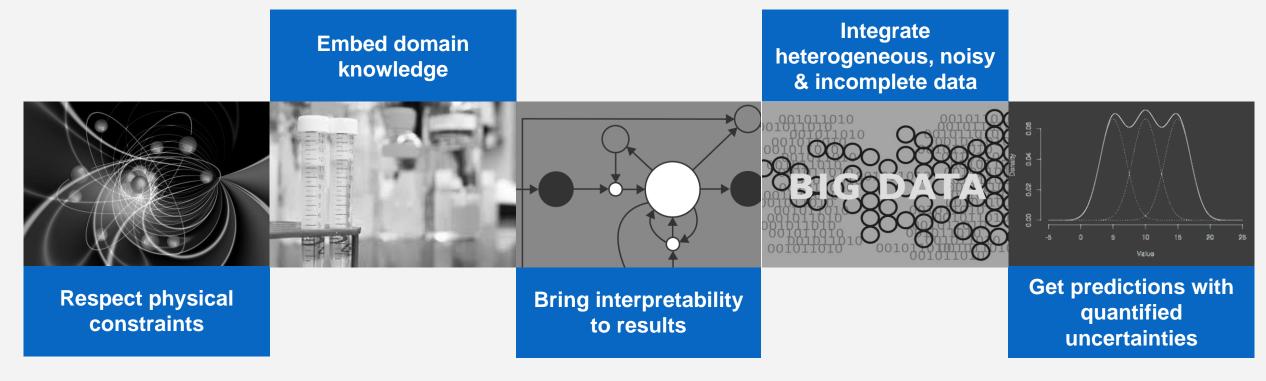
**3 Conclusions & Outlook** 

# Conclusions & Outlook

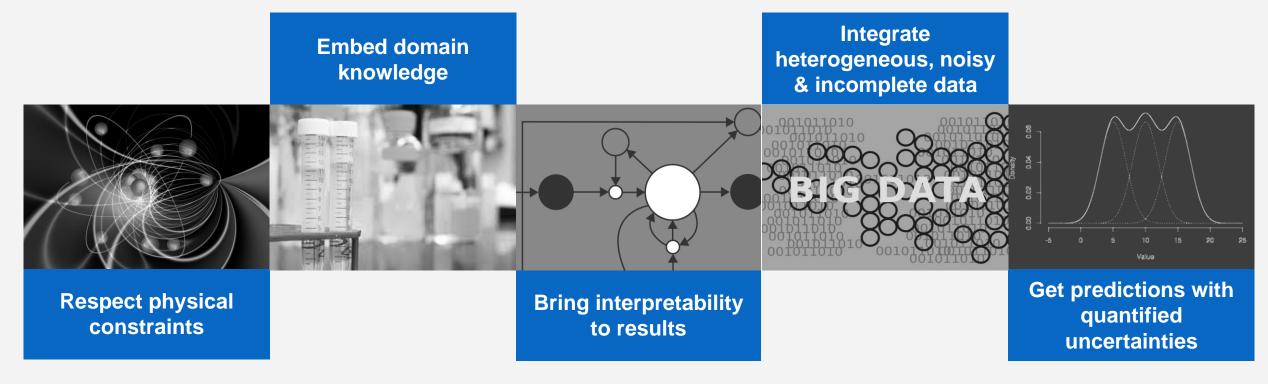
What future for model reduction?

#### What role for model reduction?

reduce the cost of training | foundational shift in ML perspectives



Learning from data through the lens of models is a way to exploit structure in an otherwise intractable problem



#### What future for model reduction?

#### Rigor

3

issuing predictions with certified uncertainty for high-consequence applications

#### 2 Relevance

towards real-world scientific and engineering applications

#### Accessibility

accessible algorithms, community software, benchmark problems

4 Impact & adoption

depend on all of the above

### **Data-driven** decisions

building the mathematical foundations and computational methods to enable design of the next generation of engineered systems

#### **KIWI.ODEN.UTEXAS.EDU**

